



UNIVERSITY OF
KWAZULU-NATAL
INYUVESI
YAKWAZULU-NATALI

SCHOOL OF ENGINEERING

EXAMINATIONS: NOVEMBER 2018

COURSE AND CODE: CHEMICAL ENGINEERING FUNDAMENTALS ENCH2EF

DURATION: 3 HOURS

TOTAL MARKS: 100

INTERNAL EXAMINERS: PROF I GOVENDER
DR K MOODLEY

INTERNAL MODERATOR: DR J POCOCK

EXTERNAL MODERATOR: DR C NARASIGADU

INSTRUCTIONS:

1. ALL questions should be attempted.
2. Two answer books are provided. Label them Book 1 and Book 2 respectively. Answer Section B in Book 1 and Section C in Book 2.
3. Any programmable or non-programmable calculator may be used provided it has been cleared of any information that would subvert the purpose of the examination.
4. Calculations must be shown in sufficient detail to illustrate your understanding of the procedure.
5. This examination question paper, together with all associated diagrams **MUST BE HANDED IN TOGETHER WITH YOUR SCRIPT.**

SECTION A**QUESTION 1 (Multiple Choice)**

- Choose that answer which in your opinion is the correct or best answer and mark (with a "X") the appropriate block on the answer sheet provided.
 - If you are *sure* of your answer, mark also the block containing the question mark.
 - Use only a PEN on your answer sheet.
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1.1 A gauge attached to a pressurised nitrogen tank reads a gauge pressure of 28 inches of mercury. If atmospheric pressure is 101 kPa, which of the following options best represents the absolute pressure in the tank?
1 inch = 2.54 cm and $g = 9.81 \text{ m/s}^2$.

- A. 196 kPa
- B. 110 kPa
- C. 195 kPa
- D. 111 kPa

1.2 A liquid having a density ρ and viscosity μ is flowing through a horizontal straight pipe of diameter D at volumetric flowrate of Q . Which of the following statements best describes the relationship between the frictional head loss (H_f) and the pipe diameter?

- | | |
|----------------------|------------------------|
| A. $H_f \propto D^3$ | B. $H_f \propto 1/D^3$ |
| C. $H_f \propto D^5$ | D. $H_f \propto 1/D^5$ |

1.3 The wall of an industrial furnace is constructed from fireclay brick of thickness h and thermal conductivity k . The steady-state operating temperature is maintained at T_1 and T_2 at the inner and out surfaces respectively. If the furnace material is replaced by one with a higher thermal conductivity, which of the following statements are false?

- A. Heat flux increases
- B. Power increases
- C. Temperature gradient increases
- D. Heat efflux increases

The following description applies to Questions 1.4 and 1.5:

A heat source emits radially outward from the main axis of a cylinder of diameter $D = 4.0$ m and length $L = 7$ m. The corresponding temperature profile as a function of radius (r) is given by:

$$T(r) = c + \frac{a}{k} \left[\frac{D^2}{4} - r^2 \right],$$

where k denotes the constant thermal conductivity of the cylinder, $a = 1 \frac{\text{J}}{\text{s}\cdot\text{m}^3}$ is a fitting constant and $c = 85^\circ\text{C}$.

1.4 The heat efflux through the boundary walls of the cylinder is:

- A. 448π
- B. 112π
- C. 56π
- D. 1190π

1.5 What is the best estimate (in SI units) of the convective heat transfer coefficient under steady-state operation at ambient room temperature?

- A. 0.067
- B. 0.047
- C. 0.160
- D. 0.167

1.6 In which of the following conditions will mass transfer occur spontaneously? C and z are concentration and distance respectively.

- | | |
|------------------|-----------------------|
| i. $dC/dz > 0$ | ii. $dC/dz < 0$ |
| iii. $dC/dz = 0$ | iv. None of the above |
- A. i & ii
 - B. iii
 - C. All of the above (i, ii, iii)
 - D. iv

- TOTAL /50/**

SECTION B**QUESTION 2**

The *rotating-cylinder viscometer* comprises of a rotating, inner solid cylinder (radius, R and length L) and a fixed outer cylindrical shell as shown in figure 1. The narrow gaps (of thickness h and d as shown in the figure) are filled with a fluid. The solid cylinder is rotating at a constant angular velocity Ω about the main cylindrical axis. Assuming a Newtonian fluid of viscosity μ in the gaps:

2.1) State the no-slip boundary conditions in the h -gap and d -gap, and hence (4)

2.2) Calculate the shear rates ($\dot{\gamma}_h$ and $\dot{\gamma}_d$) in the h -gap and d -gap respectively. (6)

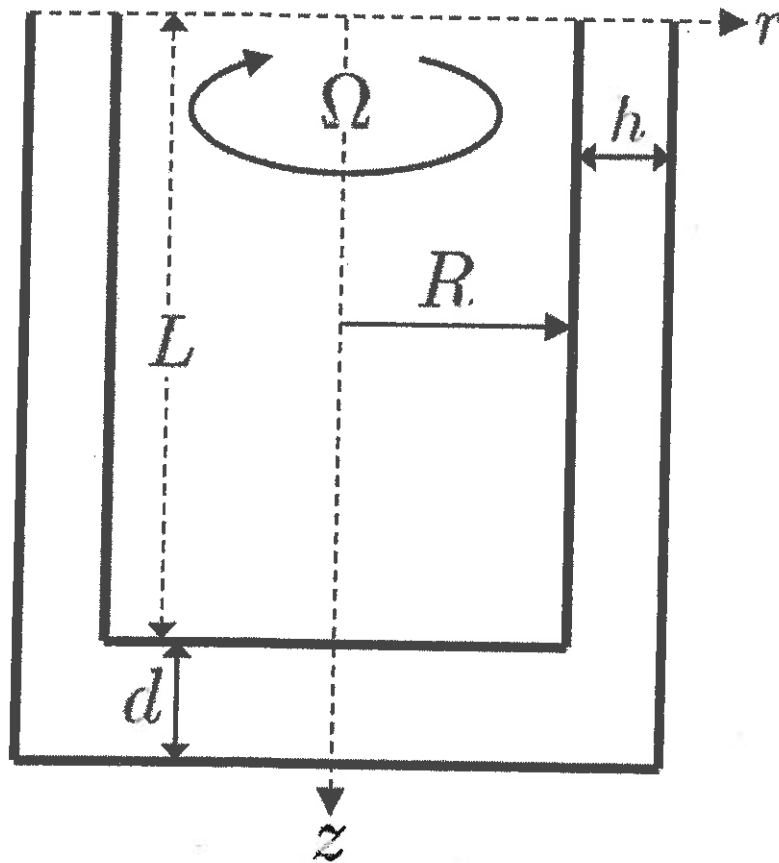


Figure 1

QUESTION 3

Consider the steady-state heat flow (without generation) through a hollow cylindrical shell with inner and outer radii r_1 and r_2 respectively. The temperatures T_1 and T_2 at the inner and outer surfaces are such that $T_1 > T_2$.

- 3.1) Describe the heat efflux $q(r)$ in the solid region. (2)
- 3.2) Describe the heat flux $\left[\frac{q(r)}{A(r)}\right]$ in the solid region. (2)
- 3.3) Obtain an expression for the heat efflux mentioned in part (3.1) in terms of r_1 , r_2 , T_1 , T_2 , L , and a constant thermal conductivity, k . (4)
- 3.4) If the thermal conductivity varies linearly with temperature as $k = a + bT$, re-derive the expression for the heat efflux. (3)
- 3.5) By comparison of the results in question (3.3) and question (3.4), obtain an expression for the *effective* thermal conductivity, k_m , for question (3.4). What is the relationship between $k = a + bT$ and k_m ? (4)

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Formula Sheet

Reynolds Number:

$$Re = \frac{Dv\rho}{\mu}$$

Newton's Law of Viscosity:

$$\tau_{rx} = -\mu \frac{dv_x(r)}{dr}$$

Mass balance:

$$\int_{cs} \rho \vec{v} \cdot d\vec{A} + \int_{cv} \rho dV = \text{Rate of mass generation}$$

Momentum balance:

$$\int_{cs} \vec{v} \rho \vec{v} \cdot d\vec{A} + \frac{\partial}{\partial t} \int_{cv} \rho \vec{v} dV = \sum \text{Forces}$$

Energy balance:

$$\int_{cs} \vec{E} \rho \vec{v} \cdot d\vec{A} + \frac{\partial}{\partial t} \int_{cv} \vec{E} \rho dV = q - \dot{W}$$

Bernoulli's Equation:

$$P + \frac{1}{2} \rho v^2 + \rho gh = \text{constant}$$

Continuity Equation:

$$\rho A v = \text{constant}$$

Enthalpy balance:

$$\bar{H}_1 + \frac{v_{1,av}^2}{2\alpha} + gy_1 \pm \bar{W}_s = \bar{H}_2 + \frac{v_{2,av}^2}{2\alpha} + gy_2 + \bar{Q}$$

Mechanical energy balance:

$$\frac{v_{1,av}^2}{2\alpha} + gy_1 + \frac{P_1}{\rho} \pm \bar{W}_s = \frac{v_{2,av}^2}{2\alpha} + gy_2 + \frac{P_2}{\rho} + \sum \bar{F}$$

Head loss balance:

$$\frac{v_{1,av}^2}{2\alpha g} + y_1 + \frac{P_1}{\rho g} \pm H_E = \frac{v_{2,av}^2}{2\alpha} + y_2 + \frac{P_2}{\rho g} + H_f$$

Power:

$$\rho g F H_E, \text{ where } F \text{ is the volumetric flowrate}$$

Hagen-Poiseuille Equation:

$$\Delta P_f = \frac{32\mu(\Delta \ell)v_{av}^2}{D^2}$$

Frictional pressure drop (any Re):

$$\Delta P_f = 2f \frac{\Delta \ell}{D} v_{av}^2, \text{ where } f \text{ is the Fanning friction factor}$$

Fourier's Law:

$$\frac{q_x}{A} = -k \frac{dT}{dx}$$

In the x-direction

Newton's Law of Cooling:

$$q = hA(T_s - T_e)$$

$$T_s > T_e$$

SECTION C**QUESTION 4**

A 20-cm-long, cylindrical graphite (pure carbon) rod is inserted into an oxidizing atmosphere at 1145 K and 1.013×10^5 Pa pressure. The oxidizing process is limited by the diffusion of oxygen counter-flow to the carbon monoxide (CO) that is formed on the cylindrical surface. Under the conditions of the combustion process, the diffusivity of oxygen in the gas mixture may be assumed to be $1.0 \times 10^{-5} \text{ m}^2/\text{s}$.

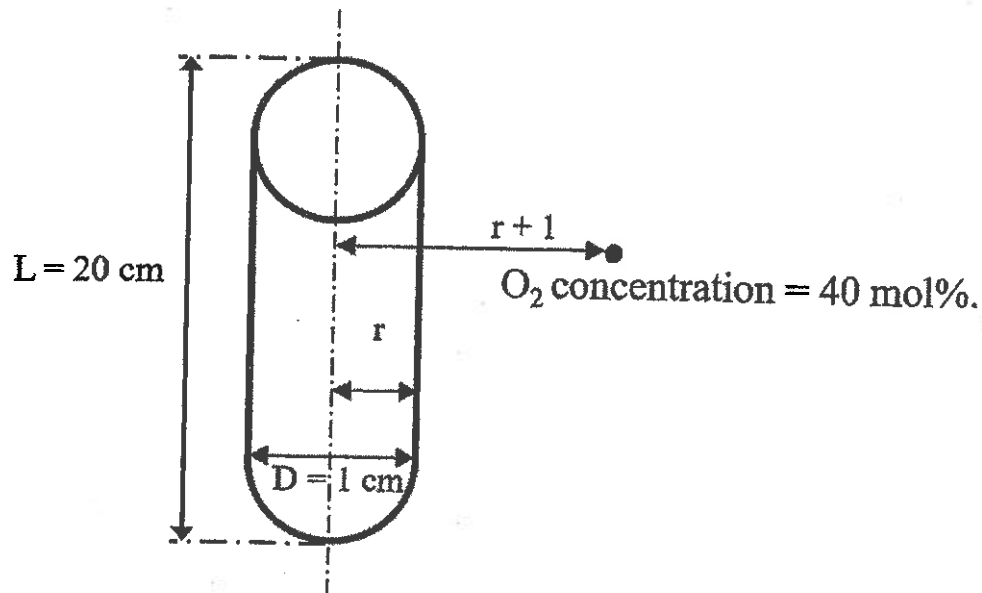


Figure 2

The combustion reaction is: $2\text{C} + \text{O}_2 \rightarrow 2\text{CO}$

- 4.1) Referring to figure 2, determine the moles of CO that are produced at the surface of the rod per second at the time when the diameter of the rod is 1.0 cm and the oxygen concentration that is a 1.0 cm distance from the rod [(1 + rod radius) cm from centre of the rod] is 40 mol%. Assume a steady-state process.

(10)

- 4.2) What would be the composition of oxygen 1.0 cm from the centre of the rod?

(7)

Question 4 continued ...

Useful equations for Question 4:

General equation for diffusion over generic distance x :

$$N_{Ax} = (N_{Ax} + N_{Bx})C_A/C - D_{AB}dC_A/dx,$$

where:

N_{Ax} is the mass flux of A in the x direction,

N_{Bx} is the mass flux of B in the x direction,

C_A is the concentration of A diffusing,

C is the concentration of the bulk fluid, and

D_{AB} is the diffusion coefficient.

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QUESTION 5

McAdams presented the heat-transfer equation for the turbulent flow of gases past a single sphere.

$$Nu = \frac{hd_p}{k} = 0.37(Re_{dp})^{0.6}(Pr^{1/3}),$$

where $Re_{dp} = \frac{d_p v_\infty}{\nu}$ with d_p the diameter of the sphere.

5.1) Propose the equation you would use to correlate the mass-transfer coefficient from a single sphere into a turbulent gas stream.

(3)

5.2) How would you modify your equation to cover a very low Reynolds number range?

(5)

Useful equations for Question 5:

General equation for diffusion over generic distance x :

$$N_{Ax} = (N_{Ax} + N_{Bx})C_A/C - D_{AB}dC_A/dx,$$

where N_{Ax} is the mass flux of A in the x direction,

N_{Bx} is the mass flux of B in the x direction,

C_A is the concentration of A diffusing,

C is the concentration of the bulk fluid, and

D_{AB} is the diffusion coefficient.

Chilton-Colburn analogy:

For heat	For mass
$\frac{f}{2} = St Pr^{\frac{2}{3}}$, where	$\frac{f}{2} = \frac{k_c}{\bar{v}} \left(Sc^{\frac{2}{3}} \right)$, where
f is the friction factor	f is the friction factor
St is the Stanton number	$\bar{v}$ is the average velocity
Pr is the Prandtl number	Sc is the Schmidt number

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